- It is nearly impossible to design a linearphase IIR transfer function
- It is always possible to design an FIR transfer function with an exact linear-phase response
- Consider a causal FIR transfer function H(z) of length N+1, i.e., of order N:

$$H(z) = \sum_{n=0}^{N} h[n] z^{-n}$$

• The above transfer function has a linear phase, if its impulse response *h*[*n*] is either **symmetric**, i.e.,

$$h[n] = h[N-n], 0 \le n \le N$$

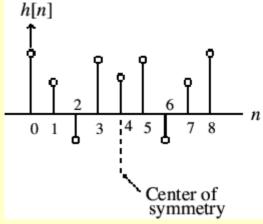
or is antisymmetric, i.e.,

$$h[n] = -h[N-n], 0 \le n \le N$$

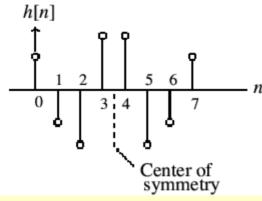
- Since the length of the impulse response can be either even or odd, we can define four types of linear-phase FIR transfer functions
- For an antisymmetric FIR filter of odd length, i.e., *N* even

$$h[N/2] = 0$$

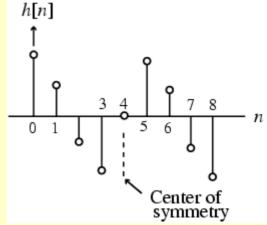
• We examine next the each of the 4 cases



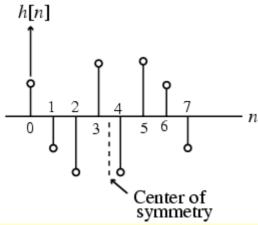
Type 1: N = 8



Type 2: N = 7



Type 3: *N*= 8



Type 4: N = 7

Type 1: Symmetric Impulse Response with Odd Length

- In this case, the degree *N* is even
- Assume N = 8 for simplicity
- The transfer function H(z) is given by

$$H(z) = h[0] + h[1]z^{-1} + h[2]z^{-2} + h[3]z^{-3}$$

+ $h[4]z^{-4} + h[5]z^{-5} + h[6]z^{-6} + h[7]z^{-7} + h[8]z^{-8}$

- Because of symmetry, we have h[0] = h[8], h[1] = h[7], h[2] = h[6], and h[3] = h[5]
- Thus, we can write

$$H(z) = h[0](1+z^{-8}) + h[1](z^{-1}+z^{-7})$$

$$+ h[2](z^{-2}+z^{-6}) + h[3](z^{-3}+z^{-5}) + h[4]z^{-4}$$

$$= z^{-4}\{h[0](z^{4}+z^{-4}) + h[1](z^{3}+z^{-3})$$

$$+ h[2](z^{2}+z^{-2}) + h[3](z+z^{-1}) + h[4]\}$$

• The corresponding frequency response is then given by

$$H(e^{j\omega}) = e^{-j4\omega} \{2h[0]\cos(4\omega) + 2h[1]\cos(3\omega) + 2h[2]\cos(2\omega) + 2h[3]\cos(\omega) + h[4]\}$$

• The quantity inside the braces is a real function of ω , and can assume positive or negative values in the range $0 \le |\omega| \le \pi$

• The phase function here is given by

$$\theta(\omega) = -4\omega + \beta$$

where β is either 0 or π , and hence, it is a linear function of ω in the generalized sense

• The group delay is given by

$$\tau(\omega) = -\frac{d\theta(\omega)}{d\omega} = 4$$

indicating a constant group delay of 4 samples

• In the general case for Type 1 FIR filters, the frequency response is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2}\tilde{H}(\omega)$$

where the **amplitude response** $H(\omega)$, also called the **zero-phase response**, is of the form

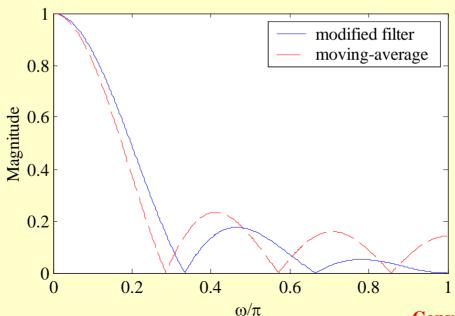
$$\tilde{H}(\omega) = h\left[\frac{N}{2}\right] + 2\sum_{n=1}^{N/2} h\left[\frac{N}{2} - n\right] \cos(\omega n)$$

• Example - Consider

$$H_0(z) = \frac{1}{6} \left[\frac{1}{2} + z^{-1} + z^{-2} + z^{-3} + z^{-4} + z^{-5} + \frac{1}{2} z^{-6} \right]$$
 which is seen to be a slightly modified version of a length-7 moving-average FIR filter

 The above transfer function has a symmetric impulse response and therefore a linear phase response

• A plot of the magnitude response of $H_0(z)$ along with that of the 7-point moving-average filter is shown below



- Note the improved magnitude response obtained by simply changing the first and the last impulse response coefficients of a moving-average (MA) filter
- It can be shown that we an express

$$H_0(z) = \frac{1}{2}(1+z^{-1}) \cdot \frac{1}{6}(1+z^{-1}+z^{-2}+z^{-3}+z^{-4}+z^{-5})$$

which is seen to be a cascade of a 2-point MA filter with a 6-point MA filter

• Thus, $H_0(z)$ has a double zero at z = -1, i.e., $(\omega = \pi)$

Type 2: Symmetric Impulse Response with Even Length

- In this case, the degree N is odd
- Assume N = 7 for simplicity
- The transfer function is of the form

$$H(z) = h[0] + h[1]z^{-1} + h[2]z^{-2} + h[3]z^{-3} + h[4]z^{-4} + h[5]z^{-5} + h[6]z^{-6} + h[7]z^{-7}$$

 Making use of the symmetry of the impulse response coefficients, the transfer function can be written as

$$H(z) = h[0](1+z^{-7}) + h[1](z^{-1}+z^{-6})$$

$$+ h[2](z^{-2}+z^{-5}) + h[3](z^{-3}+z^{-4})$$

$$= z^{-7/2} \{h[0](z^{7/2}+z^{-7/2}) + h[1](z^{5/2}+z^{-5/2})$$

$$+ h[2](z^{3/2}+z^{-3/2}) + h[3](z^{1/2}+z^{-1/2})\}$$

• The corresponding frequency response is given by

$$H(e^{j\omega}) = e^{-j7\omega/2} \{2h[0]\cos(\frac{7\omega}{2}) + 2h[1]\cos(\frac{5\omega}{2}) + 2h[2]\cos(\frac{3\omega}{2}) + 2h[3]\cos(\frac{\omega}{2})\}$$

• As before, the quantity inside the braces is a real function of ω , and can assume positive or negative values in the range $0 \le |\omega| \le \pi$

Here the phase function is given by

$$\theta(\omega) = -\frac{7}{2}\omega + \beta$$

where again β is either 0 or π

- As a result, the phase is also a linear function of ω in the generalized sense
- The corresponding group delay is

$$\tau(\omega) = \frac{7}{2}$$

indicating a group delay of $\frac{7}{2}$ samples

• The expression for the frequency response in the general case for Type 2 FIR filters is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2}\tilde{H}(\omega)$$

where the amplitude response is given by

$$\tilde{H}(\omega) = 2 \sum_{n=1}^{(N+1)/2} h[\frac{N+1}{2} - n] \cos(\omega(n - \frac{1}{2}))$$

Type 3: Antiymmetric Impulse Response with Odd Length

- In this case, the degree N is even
- Assume N = 8 for simplicity
- Applying the symmetry condition we get

$$H(z) = z^{-4} \{ h[0](z^4 - z^{-4}) + h[1](z^3 - z^{-3}) + h[2](z^2 - z^{-2}) + h[3](z - z^{-1}) \}$$

• The corresponding frequency response is given by

$$H(e^{j\omega}) = e^{-j4\omega}e^{-j\pi/2}\{2h[0]\sin(4\omega) + 2h[1]\sin(3\omega) + 2h[2]\sin(2\omega) + 2h[3]\sin(\omega)\}$$

• It also exhibits a generalized phase response given by

$$\theta(\omega) = -4\omega + \frac{\pi}{2} + \beta$$

where β is either 0 or π

The group delay here is

$$\tau(\omega) = 4$$

indicating a constant group delay of 4 samples

In the general case

$$H(e^{j\omega}) = je^{-jN\omega/2}\tilde{H}(\omega)$$

where the amplitude response is of the form

$$\tilde{H}(\omega) = 2\sum_{n=1}^{N/2} h\left[\frac{N}{2} - n\right] \sin(\omega n)$$

Type 4: Antiymmetric Impulse Response with Even Length

- In this case, the degree *N* is even
- Assume N = 7 for simplicity
- Applying the symmetry condition we get

$$H(z) = z^{-7/2} \{ h[0](z^{7/2} - z^{-7/2}) + h[1](z^{5/2} - z^{-5/2}) + h[2](z^{3/2} - z^{-3/2}) + h[3](z^{1/2} - z^{-1/2}) \}$$

• The corresponding frequency response is given by

$$H(e^{j\omega}) = e^{-j7\omega/2} e^{-j\pi/2} \{2h[0]\sin(\frac{7\omega}{2}) + 2h[1]\sin(\frac{5\omega}{2}) + 2h[2]\sin(\frac{3\omega}{2}) + 2h[3]\sin(\frac{\omega}{2})\}$$

• It again exhibits a generalized phase response given by

$$\Theta(\omega) = -\frac{7}{2}\omega + \frac{\pi}{2} + \beta$$

where β is either 0 or π

• The group delay is constant and is given by

$$\tau(\omega) = \frac{7}{2}$$

In the general case we have

$$H(e^{j\omega}) = je^{-jN\omega/2}\tilde{H}(\omega)$$

where now the amplitude response is of the form

$$\tilde{H}(\omega) = 2 \sum_{n=1}^{(N+1)/2} h[\frac{N+1}{2} - n] \sin(\omega(n - \frac{1}{2}))$$

General Form of Frequency Response

• In each of the four types of linear-phase FIR filters, the frequency response is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2}e^{j\beta}\tilde{H}(\omega)$$

• The amplitude response $\tilde{H}(\omega)$ for each of the four types of linear-phase FIR filters can become negative over certain frequency ranges, typically in the stopband

• The magnitude and phase responses of the linear-phase FIR are given by

$$|H(e^{j\omega})| = |\tilde{H}(\omega)|$$

$$\theta(\omega) = \begin{cases} -\frac{N\omega}{2} + \beta, & \text{for } \tilde{H}(\omega) \ge 0\\ -\frac{N\omega}{2} + \beta - \pi, & \text{for } \tilde{H}(\omega) < 0 \end{cases}$$

• The group delay in each case is

$$\tau(\omega) = \frac{N}{2}$$

- Note that, even though the group delay is constant, since in general $|H(e^{j\omega})|$ is not a constant, the output waveform is not a replica of the input waveform
- An FIR filter with a frequency response that is a real function of ω is often called a zerophase filter
- Such a filter must have a noncausal impulse response

- Consider first an FIR filter with a symmetric impulse response: h[n] = h[N-n]
- Its transfer function can be written as

$$H(z) = \sum_{n=0}^{N} h[n]z^{-n} = \sum_{n=0}^{N} h[N-n]z^{-n}$$

• By making a change of variable m = N - n, we can write

$$\sum_{n=0}^{N} h[N-n]z^{-n} = \sum_{m=0}^{N} h[m]z^{-N+m} = z^{-N} \sum_{m=0}^{N} h[m]z^{m}$$
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• But,

$$\sum_{m=0}^{N} h[m] z^m = H(z^{-1})$$

• Hence for an FIR filter with a symmetric impulse response of length *N*+1 we have

$$H(z) = z^{-N}H(z^{-1})$$

• A real-coefficient polynomial H(z) satisfying the above condition is called a mirror-image polynomial (MIP)

• Now consider first an FIR filter with an antisymmetric impulse response:

$$h[n] = -h[N-n]$$

• Its transfer function can be written as

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$$H(z) = \sum_{n=0}^{N} h[n]z^{-n} = -\sum_{n=0}^{N} h[N-n]z^{-n}$$

• By making a change of variable m = N - n, we get

$$-\sum_{n=0}^{N} h[N-n]z^{-n} = -\sum_{m=0}^{N} h[m]z^{-N+m} = -z^{-N}H(z^{-1})$$
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• Hence, the transfer function H(z) of an FIR filter with an antisymmetric impulse response satisfies the condition

$$H(z) = -z^{-N}H(z^{-1})$$

• A real-coefficient polynomial H(z) satisfying the above condition is called a **antimirror-image polynomial** (AIP)

- It follows from the relation $H(z) = \pm z^{-N} H(z^{-1})$ that if $z = \xi_o$ is a zero of H(z), so is $z = 1/\xi_o$
- Moreover, for an FIR filter with a real impulse response, the zeros of H(z) occur in complex conjugate pairs
- Hence, a zero at $z = \xi_o$ is associated with a zero at $z = \xi_o^*$

• Thus, a complex zero that is not on the unit circle is associated with a set of 4 zeros given by

$$z = re^{\pm j\phi}, \quad z = \frac{1}{r}e^{\pm j\phi}$$

• A zero on the unit circle appear as a pair

$$z = e^{\pm j\phi}$$

as its reciprocal is also its complex conjugate

- Since a zero at $z = \pm 1$ is its own reciprocal, it can appear only singly
- Now a Type 2 FIR filter satisfies

$$H(z) = z^{-N}H(z^{-1})$$

with degree N odd

• Hence $H(-1) = (-1)^{-N} H(-1) = -H(-1)$ implying H(-1) = 0, i.e., H(z) must have a zero at z = -1

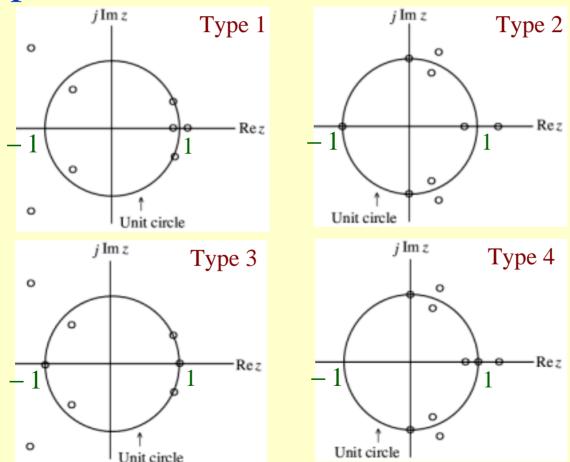
• Likewise, a Type 3 or 4 FIR filter satisfies

$$H(z) = -z^{-N}H(z^{-1})$$

- Thus $H(1) = -(1)^{-N} H(1) = -H(1)$ implying that H(z) must have a zero at z = 1
- On the other hand, only the Type 3 FIR filter is restricted to have a zero at z = -1 since here the degree N is even and hence,

$$H(-1) = -(-1)^{-N} H(-1) = -H(-1)$$

Typical zero locations shown below



- Summarizing
 - (1) Type 1 FIR filter: Either an even number or no zeros at z = 1 and z = -1
 - (2) Type 2 FIR filter: Either an even number or no zeros at z = 1, and an odd number of zeros at z = -1
 - (3) Type 3 FIR filter: An odd number of zeros at z = 1 and z = -1

- (4) Type 4 FIR filter: An odd number of zeros at z = 1, and either an even number or no zeros at z = -1
- The presence of zeros at $z = \pm 1$ leads to the following limitations on the use of these linear-phase transfer functions for designing frequency-selective filters

- A Type 2 FIR filter cannot be used to design a highpass filter since it always has a zero z = -1
- A Type 3 FIR filter has zeros at both z = 1 and z = -1, and hence cannot be used to design either a lowpass or a highpass or a bandstop filter

- A Type 4 FIR filter is not appropriate to design a lowpass filter due to the presence of a zero at z = 1
- Type 1 FIR filter has no such restrictions and can be used to design almost any type of filter

 A causal stable real-coefficient transfer function H(z) is defined as a bounded real (BR) transfer function if

 $|H(e^{j\omega})| \le 1$ for all values of ω

• Let x[n] and y[n] denote, respectively, the input and output of a digital filter characterized by a BR transfer function H(z) with $X(e^{j\omega})$ and $Y(e^{j\omega})$ denoting their DTFTs

• Then the condition $|H(e^{j\omega})| \le 1$ implies that

$$\left|Y(e^{j\omega})\right|^2 \le \left|X(e^{j\omega})\right|^2$$

• Integrating the above from $-\pi$ to π , and applying Parseval's relation we get

$$\sum_{n=-\infty}^{\infty} |y[n]|^2 \le \sum_{n=-\infty}^{\infty} |x[n]|^2$$

- Thus, for all finite-energy inputs, the output energy is less than or equal to the input energy implying that a digital filter characterized by a BR transfer function can be viewed as a **passive structure**
- If $|H(e^{j\omega})|=1$, then the output energy is equal to the input energy, and such a digital filter is therefore a **lossless system**

- A causal stable real-coefficient transfer function H(z) with $|H(e^{j\omega})|=1$ is thus called a lossless bounded real (LBR) transfer function
- The BR and LBR transfer functions are the keys to the realization of digital filters with low coefficient sensitivity